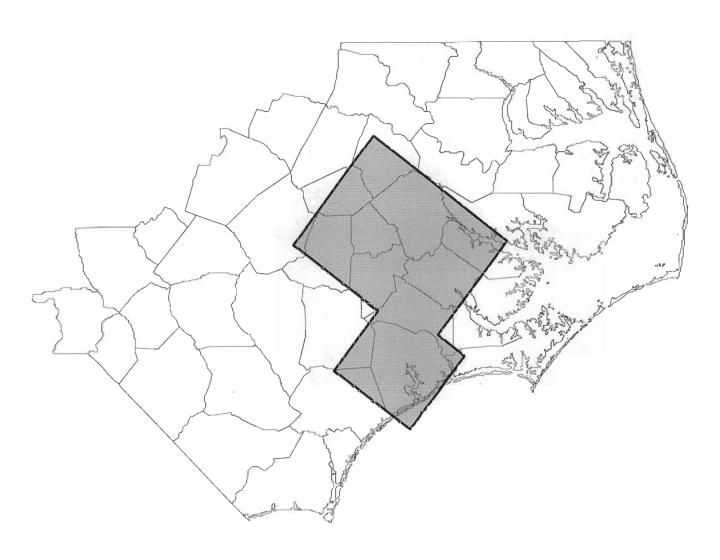
INTERIM REPORT

CENTRAL COASTAL PLAIN GROUND WATER MODEL



DIVISION OF WATER RESOURCES

April 1993

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North Carolina Department of Environment, Health, and Natural Resources

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ABSTRACT

In the past three years, the Division of Water Resources (DWR) investigated the possibility of using a ground water flow model to help local governments in the Central Coastal Plain (CCP) region of North Carolina manage their ground water use. Efforts were directed towards testing the United States Geological Survey (USGS) ground water model of the CCP developed in the late 1980s as an outgrowth of Regional Aquifer Systems Analysis work. DWR staff checked the calibration of the model by comparing actual water levels with computed water levels in the three major Cretaceous aged aquifers -- Upper Cape Fear, Black Creek, and Peedee. Model calibration during 1986-1990 time period was comparable to USGS calibration data prior to 1987 published in the USGS CCP model report. A few areas showed large discrepancies and require model recalibration for more accurate water level estimations.

Results of model runs from 1987 to 2010 show the cumulative effect of ground water pumping from the many users in the CCP area. Large cones of depression have formed and will continue to grow in depth and scope due to withdrawals in the Black Creek and Upper Cape Fear aquifers. Aquifer damage may result from lowering water levels below the top of these aquifers (dewatering) and should be avoided. Largest drawdowns occur beneath Kinston, Onslow County-Jacksonville, New Bern, and Farmville systems. The model is very capable of providing valuable information about the combined effects of all CCP water systems, however, several limitations in the model will require increased efforts by DWR and local entities to update the water use and hydrogeological data bases. An improved model can be the foundation for management of the CCP ground water resources.

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Introduction

The Central Coastal Plain region of North Carolina includes all or portions of 16 counties as illustrated on figure 1. This area has shown marked ground water level drops since the mid-1900s as ground water use has increased dramatically. The rapid lowering of ground water levels is particularly obvious in the Cretaceous¹ aged aquifers known as the Upper Cape Fear, the Black Creek, and the Peedee. The Central Coastal Plain (hereafter CCP) region includes the area of largest drawdown of ground water levels and highest population or water use growth.

The United States Geological Survey's (USGS) Regional Aquifer Systems Analysis (RASA) work began in 1978 (Winner and Coble, 1989; Giese, Eimers, and Coble, 1991). The RASA study analyzed the aquifer framework and ground water flow in the eastern coastal plain of the United States from New Jersey southward through Georgia. However, it was decided in the mid-1980s among the USGS and their cost-sharing partners that a more detailed analysis was required for the CCP because of the significant ground water use and disturbing drop in water levels.

A group of municipalities, private water systems, and county governments, the North Carolina Department of Environment, Health, and Natural Resources (EHNR), and the USGS developed a cooperative agreement which funded the CCP study. The CCP study evolved from the RASA work and involved defining the hydrogeological framework of the aquifers, recording historical withdrawals (until 1986) from the ground water system, and modeling the ground water flow through that system. The Cretaceous aquifers in the CCP were of special concern because they are extensively used for public water supplies. A complete description of the USGS model and their modeling results is found in Eimers, Lyke, and Brockman, 1990. The references at the end of this report list the major USGS reports associated with the CCP project.

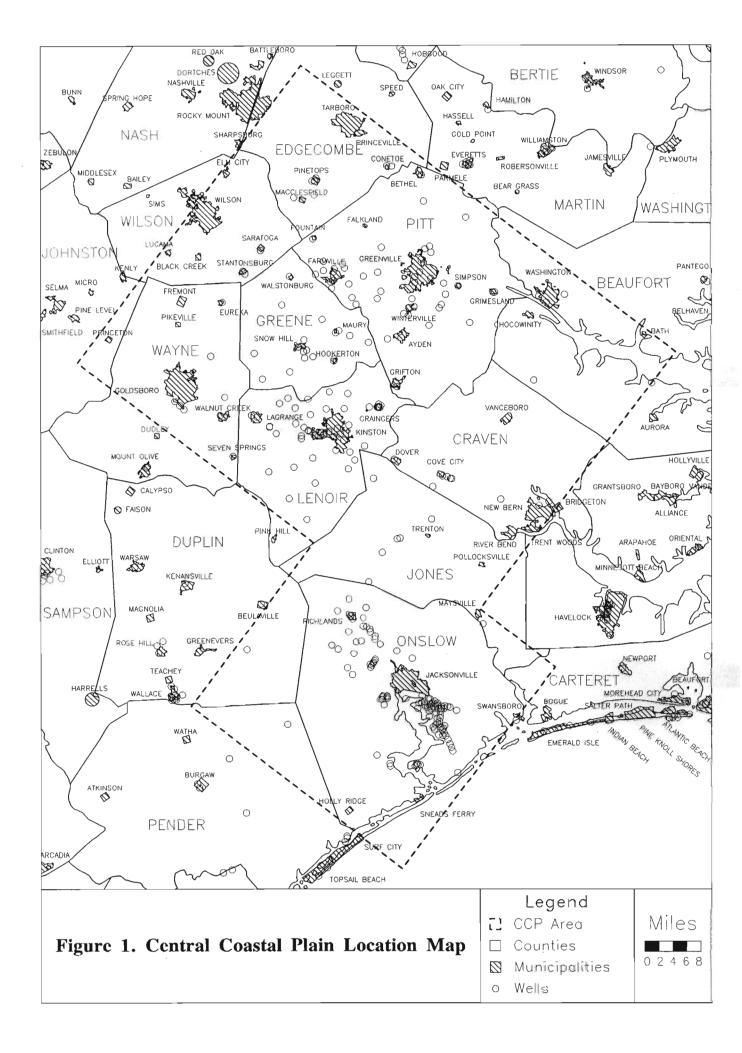
Responsibility for the ground water model operation transferred to EHNR, Division of Water Resources (DWR) in April 1990, after the USGS published their results. This report summarizes the initial efforts by DWR to use the Central Coastal Plain hydrogeological framework and an application of the ground water model developed by the North Carolina District of the USGS. The modeling results, analysis, and conclusions contained herein are the products of DWR efforts.

CCP Model Runs

Model Run Preparation

DWR has undertaken the responsibility of running the CCP model to help local governments and other water users manage the ground water resources of the area. DWR advertised the availability of the model in April 1990 as a tool to examine the effects of different rates of ground water withdrawal on the aquifer system and received responses from the following cooperators:

¹ Cretaceous is a period in the geologic time scale which refers to sediments deposited between about 144 and 66 million years before present.



Kinston, Jacksonville, New Bern, Onslow County, and Farmville. On the whole, the cooperators understood the capabilities of the model, but some exhibited misconceptions about expected results from model runs. Between the initial requests for model runs in June 1990 from Kinston and the latest from Farmville in February 1992, DWR gained a better comprehension of the ground water flow model.

The model uses a computer program developed by the USGS in the 1980s (McDonald and Harbaugh, 1988) which is commonly called MODFLOW. DWR personnel received training in the use of MODFLOW and learned valuable tips for running the CCP model from USGS hydrologists and modelers.

The modeled area is subdivided vertically into ten layers corresponding to the number of aquifers, and horizontally into 102 columns and 120 rows (figure 2). Thus, the model contains 122,400 grid cells (10 layers by 120 rows by 102 columns). About 30% of these cells are inactive because they lie outside the lateral limits of a particular aquifer or they are outside the no-flow boundaries delimited by the 10,000 mg/l chloride concentration of ground water. The density of cells is highest in the CCP area for better resolution, and decreases toward the boundaries of the model grid. Within the CCP area cell size averages 0.98 square miles with smallest cells covering 0.77 square miles. Outside the CCP area cell size reaches a maximum of 56.25 square miles. The model estimates a ground water level in each grid cell at certain time steps by calculating the flow of ground water through the cells. The ground water level in a cell is a function of a change in the amount of stored ground water, which is equal to the difference between the amount of ground water flow into the cell from neighboring cells and through recharge, and the amount of ground water flow out of each cell by wells and from discharge to neighboring cells.

DWR gathered additional water use data from many of the larger ground water users in the Central Coastal Plain region to estimate the withdrawal of ground water between 1986 and 1991. Detailed information for most of the water systems in the area was gained from Water Supply System Report for 1989 questionnaires previously completed and returned to DWR and through additional data requests by DWR to specific communities and industries.

Three model runs were completed in July and August of 1992 using water use data collected by DWR in 1990, 1991, and early 1992. Each of these runs required time-consuming efforts (typically 2 to 3 weeks) to create the input data file, transfer it via modem to the USGS computer system, run the model (3-5 day run-time), transfer the necessary output data back to DWR computers via modem, and analyze the output. In January of 1993 DWR moved the model to a computer within the Division to allow more efficient runs.

Model Calibration

In order to test the accuracy of the CCP model, actual water levels must be compared to computed values. Levels from seven EHNR research station wells were chosen for this process and are illustrated on figure 3. These research stations were picked because of their distinct geographic positions (figures 13-15) and the aquifer each sampled. It should be noted that yearly average water levels for these monitoring wells are charted against calculated water levels from the center of the model cell encompassing the well location. If the research station well lies near the perimeter of the cell, then some differences between the two levels may exist.

In general, computed water levels track actual variation in water levels between 1986 and 1990 as

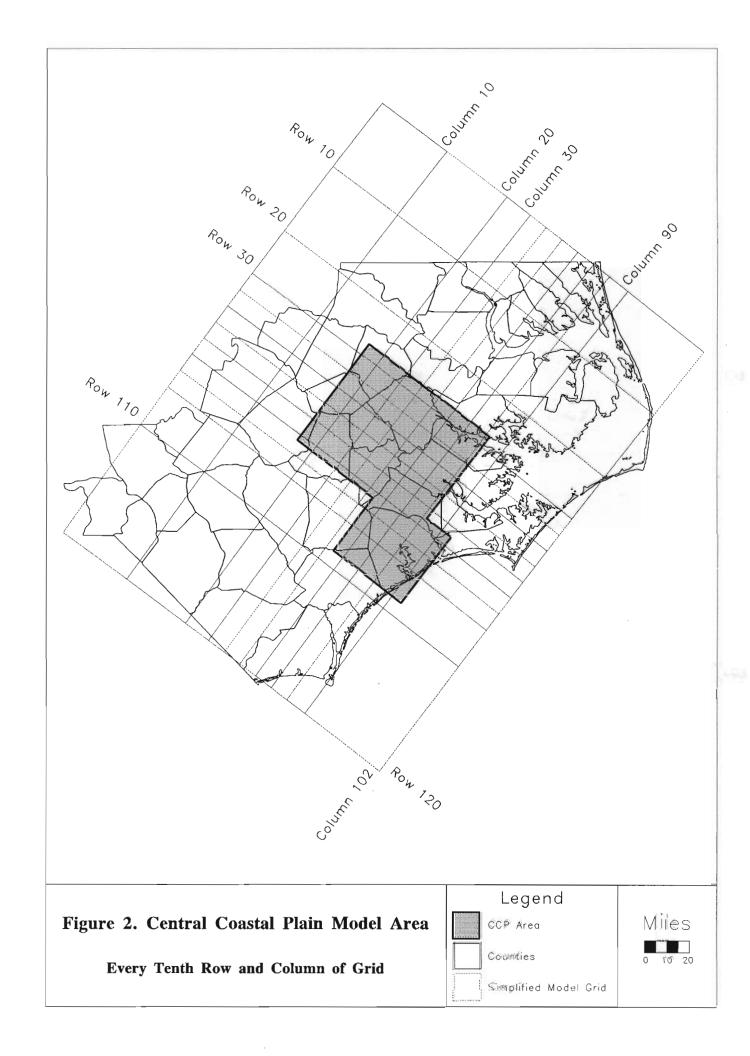
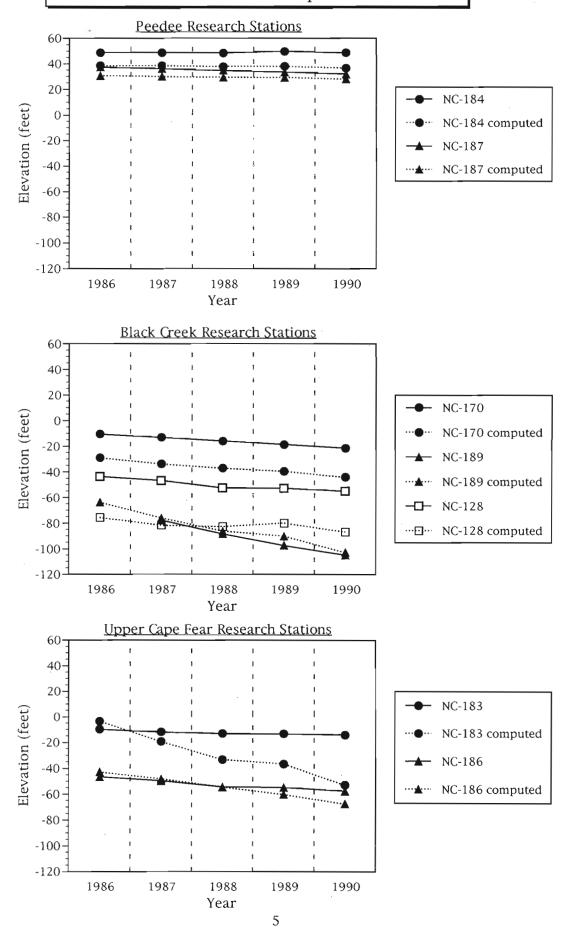


Figure 3. Yearly Average Ground Water Elevation Actual versus Computed



well as was described in the USGS model report for water levels prior to 1987 (Eimers, Lyke, and Brockman, 1990). In most cases, the computed level follows the proper trend, but at a lower elevation. The differential ranges from about 5 to 35 feet. The largest deviations occur in the more heavily pumped aquifers -- the Black Creek and Upper Cape Fear aquifers. The two most significant comparisons occur with NC-128 and NC-183.

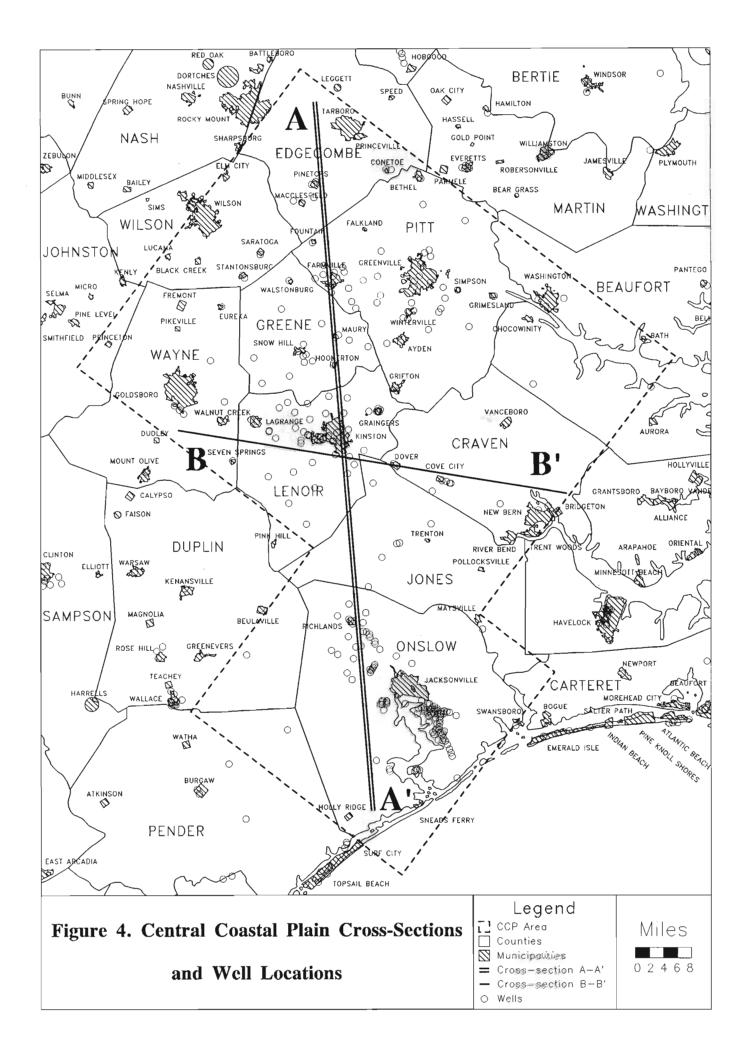
The Black Creek research station near Kinston (NC-128) shows significantly higher water levels than the computed values for that model cell. In this case, as well as with NC-183, model parameters need to be adjusted to produce levels in line with the actual conditions. Research station NC-183, which lies northeast of Farmville, gives water level information vastly different than the model estimates. In fact, the levels are diverging. Limited water level data from Farmville seems to follow the research station trend. Both of these cases NC-183, and NC-128 suggest that recalibration in these areas is necessary prior to estimating where and when water levels might drop below the top of the aquifer and cause aquifer de-watering.

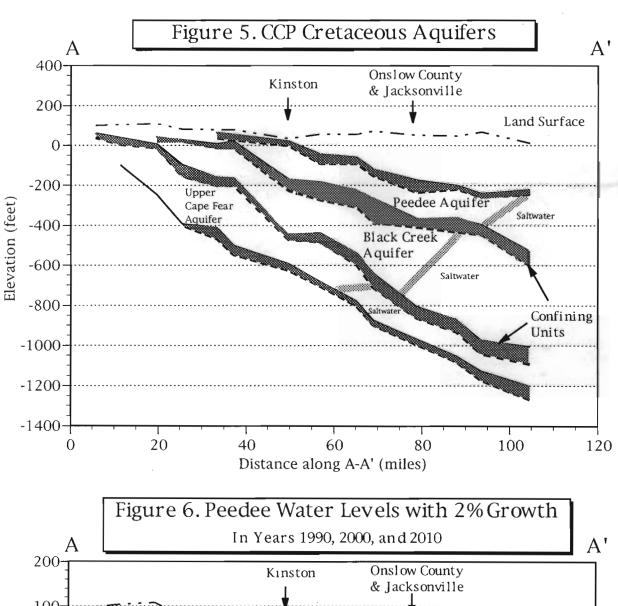
Model Results

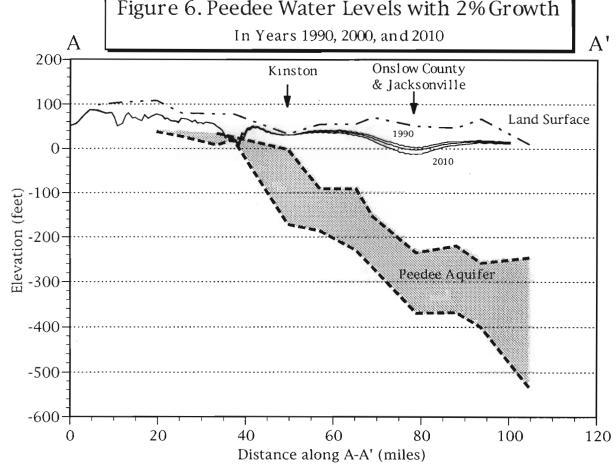
The three DWR model runs estimated ground water levels for the Cretaceous aquifers in the CCP region. Results are presented for the Peedee, Black Creek, and Upper Cape Fear aquifers. The first run used a two percent growth in water use per year, the second incorporated a linear trend to estimate future water use, and the third assumed no increased water withdrawals beyond latest water use figures (latest use ranged from 1986 to 1991 values). Each model run estimated ground water levels until the year 2010 in five-year increments, or stress periods. The average volume pumped per grid cell for each five-year stress period was used in the computations. Rates of ground water use by the CCP cooperators are listed in Appendix A (water use by the 140 other users represented in the model are not included in this appendix). Values for each model run are tabulated by year and by stress period.

The two-percent growth simulation results are illustrated on the attached figures 6-8 and 10-12. This growth rate most accurately reflected total water use growth in the CCP between 1986 and 1991. Results from the second run using linear growth were discarded because of errors. This method of linear extrapolation of ground water withdrawals proved to be inaccurate because of gaps in water use records for individual wells. Although water systems can usually report total use by well field accurately, the data for individual wells is frequently not available. Thus, this missing data often skewed the calculated future water use.

One method of viewing results from model runs is to use cross-sections through an area of interest. Two cross-section lines (A-A' and B-B') were chosen for analysis and are shown along with well locations in figure 4. On figures 5 and 9, the Cretaceous aquifers of interest and their corresponding confining units are illustrated for each of these cross-sections. These are known as confined aquifers because ground water flows easily through the sand-rich, aquifer material, but flow into less permeable, clay-rich, confining material above and below the aquifer is hampered. Unconfined aquifers lack the upper confining material. Land surface and aquifer levels are drawn based on data from selected wells located near the cross-section lines. The 250 mg/l chloride concentration, delineating the boundary between freshwater and saltwater, is also shown in figures 5 and 9. This interface is based on RASA work (Winner and Coble, 1989). Chloride concentrations increase down dip towards 10,000 mg/l and eventually seawater concentrations (about 19,000 mg/l). The 10,000 mg/l concentration interface is not shown.







Figures 6-8 display, along cross-section A-A´, water levels for the Peedee, Black Creek, and Upper Cape Fear Aquifers in the simulated years 1990, 2000, and 2010. These cross-sections indicate the rate of growth of the cone of depression from 1990 to 2010. Near Kinston for the Black Creek aquifer and Farmville for the Upper Cape Fear aquifer, it is apparent that ground water withdrawals increasing at two percent per year may cause water levels to drop below the top of the aquifer and begin to de-water the aquifer. Although, the Onslow County-Jacksonville area does not appear to be in danger of aquifer de-watering, they may experience saltwater intrusion.

De-watering may cause irreparable damage to the aquifer. Ground water is contained in the pore spaces of the aquifer material and helps support the structure of the aquifer. As ground water is drained from the aquifer, the aquifer material may compact, reducing the volume of the pore space. If water is allowed to fill the aquifer again through reduction of pumping, less water can be stored in the aquifer if pore spaces have collapsed. So, de-watering of the aquifer may cause loss in storage capacity. Also, the compaction of aquifer material may result in subsidence of the land surface.

Figures 10-12, illustrating cross-section B-B', show similar trends to the previous figures. Ground water levels are lowered dramatically near Kinston and Cove City in both the Black Creek and Upper Cape Fear aquifers. Peedee aquifer water levels show little deviation from 1990 values.

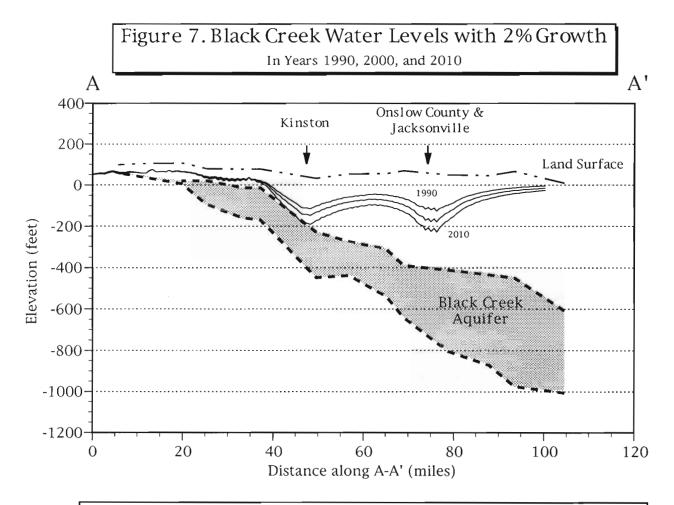
In general, the cross-sections indicate that drawdown in water levels is significant over a large region. Withdrawals from many municipal and industrial supply wells contribute to the depressed water levels. The model shows clearly the cumulative effect of the many withdrawal sites in the CCP area. This continued drawdown will require pumps be dropped to lower levels and/or new wells be drilled as has happened in the past for many CCP communities and industries. The drawdowns illustrated in these cross-sections dramatize the finite water resources available.

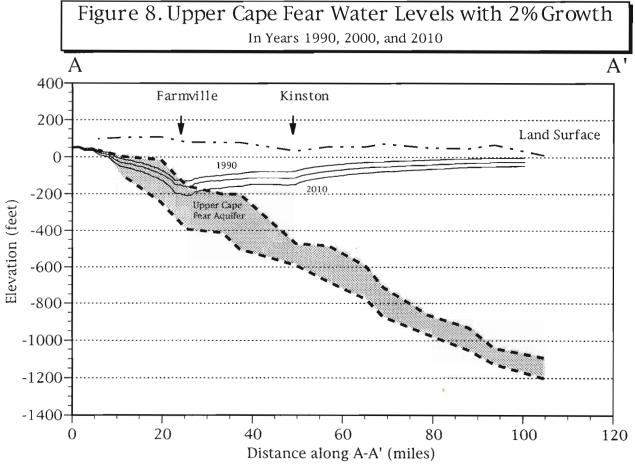
Figures 13-15 show the extent of drawdown between the years 1990 and 2010 in map format. Both the Black Creek and Upper Cape Fear aquifers show regions of high drawdown. In the Black Creek aquifer, drawdown is largest in the area between Onslow County-Jacksonville and Kinston. The Upper Cape Fear aquifer also shows widespread drawdown, with peak drawdown zones near Kinston and Farmville-Greenville. The Peedee aquifer shows only small drawdown effects over this time span assuming two-percent growth. The minor zones of drawdown occur near Onslow County-Jacksonville and Aurora. The drawdown near Aurora is due to pumping of the Castle Hayne aquifer (an aquifer above the Peedee) at Texas Gulf, Inc.

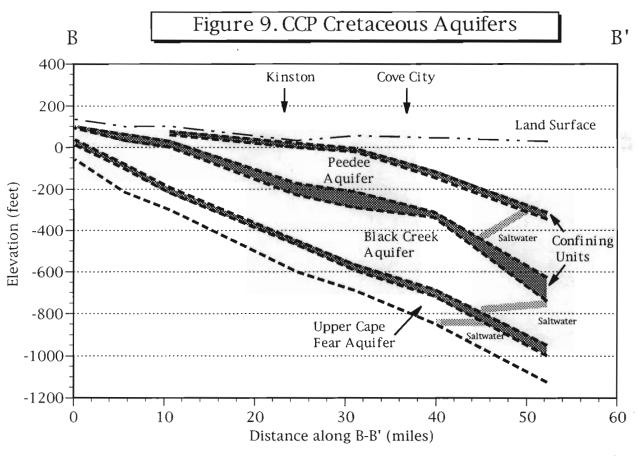
The third simulation incorporating no growth in water withdrawals was run to determine if ground water levels would reach equilibrium at 1986 to 1991 (depending on data from system) withdrawal rates. According to the model, if pumping is sustained at these rates, ground water levels in the Cretaceous aquifers would stop falling and reach a balanced condition by about 2010. Further model runs were not performed that might estimate the maximum rates of withdrawal these aquifers could handle.

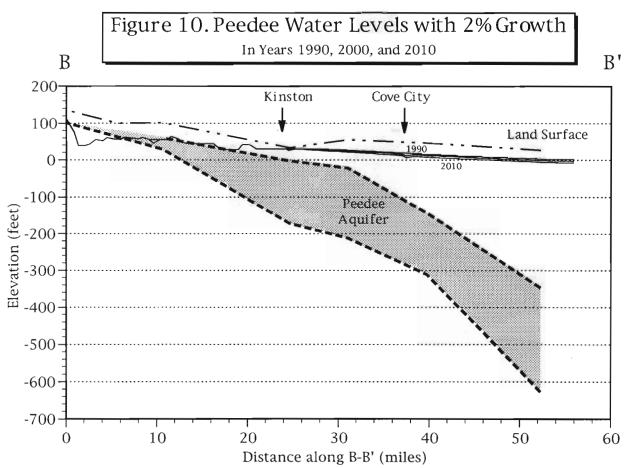
Future of CCP Model

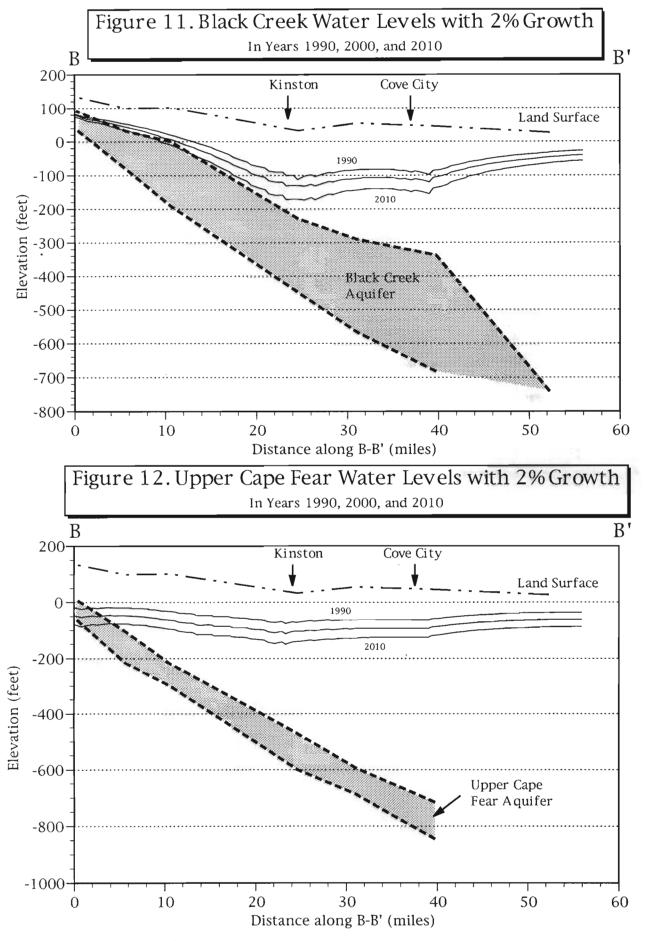
In its present state, the model is capable of estimating the cumulative effect on the water levels in the Cretaceous aquifers due to ground water withdrawals. The computer model can also be used to judge the relative merits of locating a well in one place or another (which location enlarges the cone of depression least). However, the model has a resolution of, at best, 0.8 mile because of the size

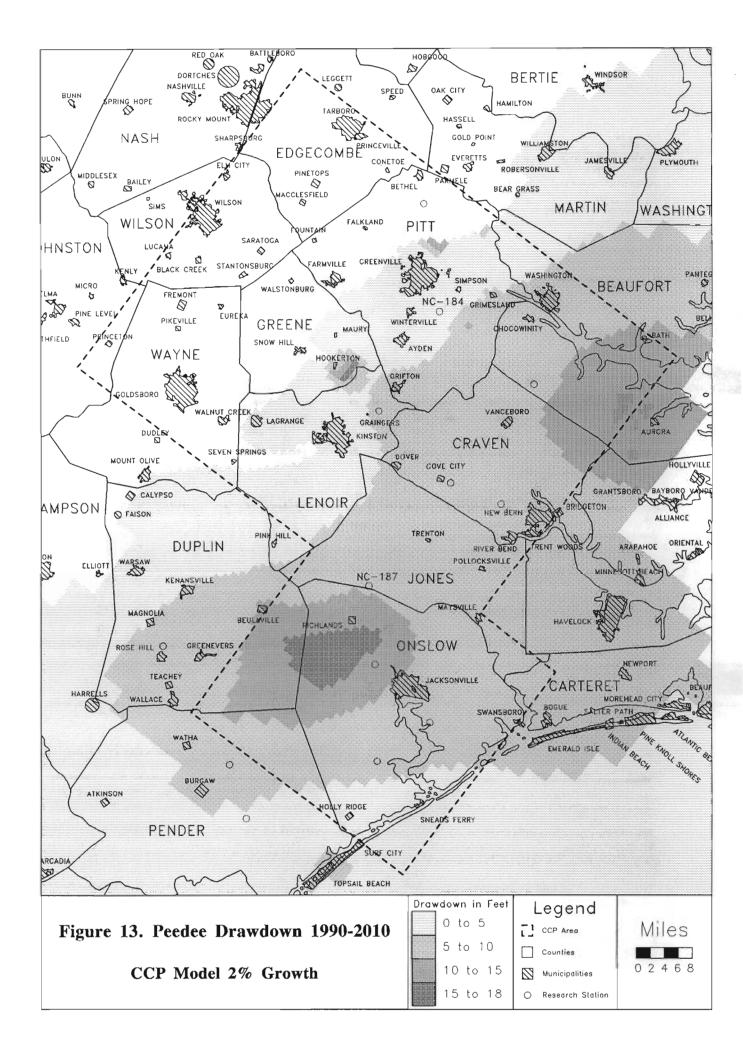


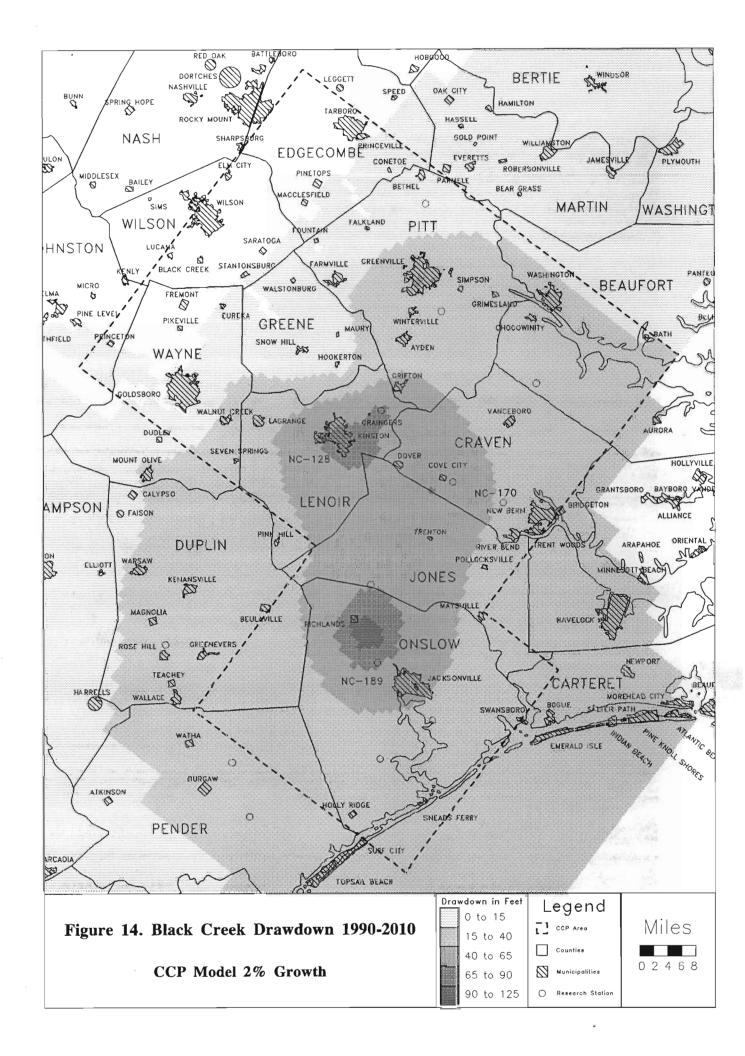


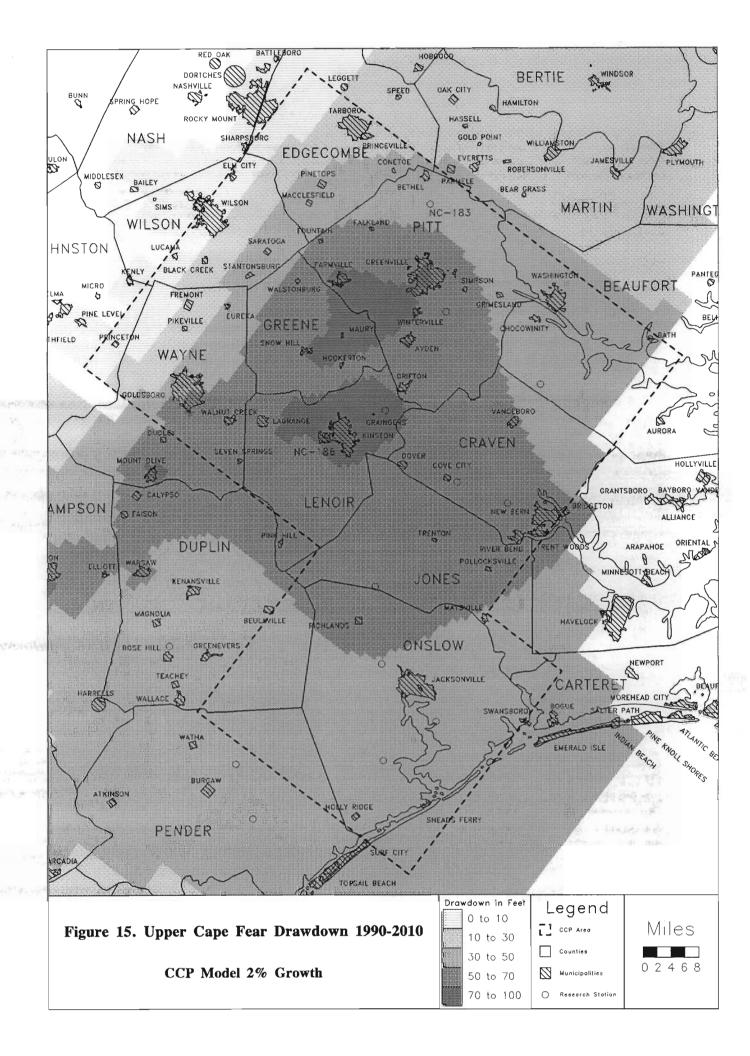












of individual grid cells. Although some cooperators hoped, it is not possible for the model to project well yield or to determine precisely the best depth, spacing, or specific location for a new well.

The previous drawdown maps and cross-sections illustrate several limitations to the model. Major limitations are described below. They are ordered from least to most difficult to overcome.

Model Limitations

- 1. The model simulates ground water flow through the aquifers without complete information about each aquifer's physical extent. This simplification greatly eases the job of developing the input data sets. Input data defines the modeled area as having ten aquifers, and assigns the relative position of each aquifer with reference to the other aquifers; the model defines layer 1 as being above layer 2, etc. However, the depths and thicknesses of each aquifer are not required. When actual physical boundaries to the aquifers are then compared to model results, as in the previous cross-sections, the hydrogeological parameters used to define ground water flow in a particular aquifer are shown to be in error. This situation is illustrated in figure 8 and corroborated by monitoring well levels from NC-183 (figure 3). According to the simulation, de-watering of the Upper Cape Fear aquifer has been occurring near Farmville since 1990; the water level in the Upper Cape Fear aquifer is below the top of the aquifer. This is known not to be the case. The solution to this limitation is to use more of the aquifer framework information when developing model runs and recalibrate the model in problem areas.
- 2. The use of a no-flow boundary at the 10,000 mg/l chloride concentration is another simplification of the aquifer system. The USGS used 10,000 mg/l chloride because no ground water users in the CCP area pump near this boundary (Eimers, Lyke, and Brockman, 1990). In the drawdown maps the eastern edge of the modeled area is this no-flow boundary. However, across that interface in several areas (and in all three aquifers) the model shows a difference in head, or as in the drawdown maps, a positive drawdown. If this is truly the case, then the no-flow boundary is not appropriately located; the boundary should be moved eastward away from the stresses to the aquifer system. Because this model boundary is too close to areas of heavy pumping, the model calculates the drawdown as greater than it really is. This exaggeration of drawdown will get larger as the stresses on the aquifer increase.
- 3. The final, significant weakness of the CCP model, in its use as a management tool, occurs in its inability to simulate saltwater intrusion. It is important to be able to estimate the effects of pumping on the rate of saltwater advancement. Onslow County and Jacksonville water systems are especially susceptible to saltwater contamination of supply wells. If modeling of the saltwater flow using a different ground water flow model proves to be too difficult or costly, then wells should be monitored to track the movement of this threat.

Some of the model's limitations could be overcome with additional effort from DWR and the local cooperators to improve the data bases for hydrogeology and water use. Certainly, more industrial and agricultural ground water users should be included in the model. No-flow boundaries could be adjusted and aquifer depth and thickness defined to increase the accuracy of the model output. Additional research stations might be constructed to verify model input data. It may be possible to transfer the data sets into another ground water flow model capable of simulating both freshwater

and saltwater. In this way, saltwater intrusion rates could be estimated.

Model Uses

It may be possible in the future to answer questions about saltwater intrusion and water levels expected from certain growth scenarios with confidence. However, the existing model provides valuable insights to understanding the far reaching effects of pumping from all CCP water systems. At the same time, the model shows incremental changes to depressed ground water levels associated with an individual water system. Information derived from using the model can therefore assist in managing and protecting the ground water resources of the region.

Conclusions

Ground water withdrawals from the Central Coastal Plain aquifers cannot be expanded without limits. The regulating factors include economic and hydrogeological concerns. Future costs of new well construction and pump lowering may put significant pressure on municipal or industrial budgets. The model strongly suggests that the cumulative withdrawals from these aquifers may cause drawdowns of the water levels to the point of harming the aquifer yields through dewatering. Although the possible effects of de-watering of the these aquifers as described earlier is uncertain, evidence from other areas in the United States suggests that de-watering should be avoided. The basis for achieving the most effective management lies with understanding the ground water resource and its limits, and with use of models that simulate the response of that resource to changing withdrawal patterns. Although the CCP model appears to be inaccurate in some areas, it can be improved to be a useful tool to allow proper planning of water resource development.

Recommendations

- 1. Ground water withdrawals should be planned to maintain the long range productivity of the CCP aquifers by avoiding aquifer de-watering.
- 2. Water users in the CCP region and the Division of Water Resources should cooperate to collect accurate data and to improve the model to provide a sound basis for regional ground water management and protection.
- 3. Water users in the CCP region should develop future water supply plans under the provisions of G.S. 143-355(l). These plans should consider available supplies from the Cretaceous aquifers, alternative water supply sources, and water conservation as means to assure adequate water supplies for future economic development.

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Appendix A. Projected Well Pumping (in MGD) by Cooperator Systems for Three Model Runs

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8661E Z6		91 0.603	enod 3 (19	0.906 0.9	eriod 3 (19		eniod 3 (19		85 2.331	eriod 3 (19	2.683 2.771	eriod 3 (19	2.011 2.011	eriod 3 (19		0.128 0.130	eriod 3 (19		eriod 3 (19	03 0.103	enod 3 (19		2.617 2.668	eriod 3 (19	52 3.297	eriod 3 (19	2.191 2.191	eriod 3 (19			
76619 P1997		0.579 0.591	Stress P	0.859 0.9	Stress P	0.505 0.505	Stress P		2.240 2.285	Suess P	2.603 2.6	Stress P	2.011 2.0	Suess P		0.126 0.1	Stress P	0.217 0.227	Suess P	0.103 0.103	Stress P		2.564 2.6	Stress P	3.001 3.152	Suress P	2.191 2.1	Suess P			
37 <u>36614</u>		0.570 0.3	0.547	0.807 0.3	902.0	0.505 0.3	0.505		2.199	2.113	2.540 2.0	2.383	2.011 2.	2.011		0.123 0.	0.118	0.208 0	0.189	0.103 0.	0.103		2.515 2.	2.418	2.857 3.	2.617	2.191 2.	2.191			_
P1994 P15		0.557 0.5		0.755 0.8		0.505 0.5			2.154 2.1		2.474 2.5		2.011 2.0			0.120 0.		0.197 0.3		0.103 0.			2.465 2.5		2.737 2.8		2.191 2.				
14 £6614		0.546 0.	Stress Period 2 (1991-1995):	0.708 0.	Stress Period 2 (1991-1995):		Stress Period 2 (1991-1995):		2.112 2.	Stress Period 2 (1991-1995):	2.411 2.	Stress Period 2 (1991-1995):	2.011 2.	Stress Period 2 (1991-1995):		0.119 0.	Stress Period 2 (1991-1995):	0.189 0.	Suess Period 2 (1991-1995):	0.103 0.	Stress Period 2 (1991-1995):		2.418 2.	Stress Period 2 (1991-1995):	2.615 2.	Suess Period 2 (1991-1995):	2.191 2.	Stress Period 2 (1991-1995):			
I 76614		0.537 0	Period 2 (0.656 0	Period 2 (0.505 0.505	Period 2 (2.071 2	Period 2 (2.353 2	Period 2 (2.011 2	Period 2 (0.117 0	Period 2	0.179 0	Period 2	0.103 0	Period 2		2.369 2	Period 2	2.496 2	s Period 2	2.191 2	s Period 2			
H 16614		0.525	Stress	0.604	Sues	0.505	Sues		2.029	Sues	2.138	Stress	2.011	Sues		0.113	Sues	0.170	Sues	0.103	Stress		2.322	Sues	2.378	Sues	2.191	Sues			
P1990 I		0.516	0.470	0.557	0.480	0.505	0.467		2.286	2.271	2.336	2.284	2.278	2.269		0.112	0.108	0.161	0.147	0.103	0.103		2.276	2.135	2.256	2.102	2.191	2.093			_
P1989		0.505		0.505					2.405		2.405	3006	2.405	:(066		0.109		0.152		0.103			2.233		2.146	:(066	2.191	:(066			
P1988		0,406 0.453	Stress Period 1 (1987-1990):	0.354 0.406 0.453	Stress Period 1 (1987-1990):	0.354 0.406 0.453 0.505	Suess Period 1 (1987-1990):		2.198	Suess Period 1 (1987-1990):	2.198	Suess Period 1 (1987-1990):	2.198	Stress Period 1 (1987-1990):		0.107	Stress Period 1 (1987-1990):	0.143	Stress Period 1 (1987-1990):	0.103 0.103 0.103	Stress Period 1 (1987-1990):		2.089	Stress Period 1 (1987-1990):	2.051	Stress Period 1 (1987-1990):	2.062 2.191	Stress Period 1 (1987-1990):			
P1987			ress Period	0.406	ress Period	0.406	ress Period		2.196	ress Period	2.196	ress Peniod	1.641 2.196	ress Períod		0.103 0.105 0.107	ress Period	0.103 0.133	ress Period	0.103	ress Ретіос		1.800 1.943	ress Period	1.800 1.954	ress Penoc	1.800 1.929	ress Period			
P1986		0.354	St	0.354	St	0.354	St		3.	St	1.6	St	1.62	St			St	0.103	St	0.103	S			St	1.800	St	1.800	S			
Yield		4.612							5.017							0.000							3.492								
# of wells		7							13							₹							17								
		t Growth		Linear Growth		No Growth			t Growth		Linear Growth		No Growth			t Growth		Linear Growth		No Growth			d Growth		Linear Growth		No Growth				
Model Run		Two-percent Growth		Linea		ž		LE	Two-percent Growth		Linea		ž		GREENE COUNTY	Two-percent Growth		Linea		ž		LLE	Two-percent Growth		Linea		Ž				
Name	AYDEN	Τ						FARMVILLE	H						ENE	Ţ						GREENVILLE	Т								

Name. Model Run # of wells JACKSONVILLE	Yield	Z861 5861d	2861A 8861A Z	0661G	a 7661a 7661a 7661a 1661a	IA 5661A	Z661A 9661A	P1998 P1999	P2000	P2001 P2002 P2003 P2004	P2005	600ZA 800ZA Z00ZA 900ZA	9 P2010
Two-percent Growth 17	8.640	3.073 2.93	2.938 3.110 3.236	3.551	3.922 4.000 4.083 4.163	4.245 4	4.331 4.415	4.503 4.593	4.687	4.782 4.875 4.975 5.074	5.174	5.279 5.383 5.492 5.602	5.713
		Stress Per	Stress Period 1 (1987-1990):	3.209	Suess Period 2 (1991-1995):	4.083	Stress Period	Stress Period 3 (1996-2000):	4.506	Stress Period 4 (2001-2005):	4.976	Suess Period 5 (2006-2010):	5.494
Linear Growth		3.073 2.954	4 3.135 3.268	3.591	3.970 3.620 3.781 3.948	4.120 4	4.315 4.526	4.739 4.953	5.163	5.379 5.592 5.804 6.017	6.230	6.471 6.729 6.986 7.245	1057 21
		Stress Per	Stress Period 1 (1987-1990):	3.237	Stress Period 2 (1991-1995):	3.888	Stress Period	Stress Period 3 (1996-2000):	4.739	Suess Period 4 (2001-2005):	5.804	Stress Period 5 (2006-2010):	986.9
No Growth		3.073 2.935 3.105	15 3.105 3.228	3.540	3.908 3.908 3.908	3.908	3.908 3.908	3.908 3.908	3.908	3.908 3.908 3.908 3.908	3.908	3,908 3,908 3,908 3,908	3.908
		Stress Per	Stress Period 1 (1987-1990):	3.202	Suess Period 2 (1991-1995):	3.908	Stress Period	Stress Period 3 (1996-2000):	3.908	Stress Period 4 (2001-2005):	3.908	Suess Period 5 (2006-2010):	3.908
JONES COUNTY													
Two-percent Growth 6	2.736	0.446 0.435	15 0.422 0.411	0.419	0.426 0.435 0.447 0.455 (0.463 0	0.471 0.480	0.492 0.501	0.510	0.522 0.531 0.544 0.553	0.567	0.576 0.589 0.598 0.612	12 0.621
		Stress Pe.	Stress Period 1 (1987-1990):	0.422	Stress Period 2 (1991-1995):	0.445	Stress Period	Suess Period 3 (1996-2000):	0.491	Stress Period 4 (2001-2005):	0.543	Stress Period 5 (2006-2010):	0.599
Linear Growth		0.446 0.435	15 0.422 0.411	0.400	0.387 0.376 0.365 0.352 (0.341 0	0.330 0.317	0.306 0.295	0.282	0.271 0.260 0.247 0.236	0.225	771.0 0.190 0.171	991:0 24
		Stress Pel	Suess Penod 1 (1987-1990):	0.417	Stress Period 2 (1991-1995):	0.364	Stress Period	Stress Period 3 (1996-2000):	0.306	Suess Period 4 (2001-2005):	0.248	Suess Period 5 (2006-2010):	0.189
No Growth		0.446 0.43	0.446 0.435 0.422 0.411	0.411	0.411 0.411 0.411 0.411 (0.411 0	0.411 0.411	0.411 0.411	0.411	0.411 0.411 0.411 0.411	0.411	0.411 0.411 0.411 0.411	11 0.411
		Stress Pe.	Suess Period 1 (1987-1990):	0.420	Stress Period 2 (1991-1995):	0.411	Stress Period	Stress Period 3 (1996-2000):	0.411	Stress Period 4 (2001-2005):	0.411	Stress Period 5 (2006-2010):	0.411
KINSTON													
Two-percent Growth 18	14.531	4.655 5.010	10 4.869 4.481	4.457	4.567 4.657 4.750 4.846	4.943 5	5.042 5.143	5.246 5.351	5.457	5,567 5.680 5.792 5.908	6.028	6.148 6.269 6.395 6.522	12 6.654
		Stress Pe.	Stress Period 1 (1987-1990):	4.704	Suess Period 2 (1991-1995):	4.753	Stress Period	Stress Period 3 (1996-2000):	5.248	Suess Period 4 (2001-2005):	5.795	Stress Period 5 (2006-2010):	6.398
Linear Growth		4.655 5.010	10 4.869 4.481	4.457	4.289 4.151 4.003 3.865	3.725 3	3.649 3.622	3.608 3.592	3.577	3.564 3.553 3.561 3.570	3.579	3.589 3.598 3.608 3.622	3.666
		Stress Pe.	Suess Period 1 (1987-1990):	4.704	Suess Period 2 (1991-1995):	4.007	Stress Period	Stress Period 3 (1996-2000):	3.610	Stress Period 4 (2001-2005):	3.565	Stress Period 5 (2006-2010):	3.617
No Growth		4.655 5.010 4.869	10 4.869 4.481	4.457	4,567 4,567 4,567 4,567	4.567 4	4.567 4.567	4.567 4.567	4.567	4.567 4.567 4.567 4.567	4.567	4.567 4.567 4.567 4.567	57 4.567
		Stress Pe	Stress Period I (1987-1990):	4.704	Stress Period 2 (1991-1995):	4.567	Stress Period	Stress Period 3 (1996-2000):	4.567	Suess Period 4 (2001-2005):	4.567	Suess Period 5 (2006-2010):	4.567
La grange													
Two-percent Growth 8	4.320	0.419 0.394	94 0.370 0.479	0.486	0.497 0.507 0.518 0.526	0.540 0	0.550 0.558	0.572 0.583	0.597	0.604 0.619 0.630 0.644	0.659	0.670 0.684 0.697 0.712	12 0.724
		Stress Pe.	Suess Period 1 (1987-1990):	0.432	Suess Period 2 (1991-1995):	0.518	Stress Period	Stress Period 3 (1996-2000):	0.572	Stress Period 4 (2001-2005):	0.631	Stress Period 5 (2006-2010):	0.697
Linear Growth		0.419 0.398	98 0.376 0.353	0.331	0.308 0.286 0.263 0.241 (0.218 0	0.196 0.173	0.151 0.128	0 126	0.129 0.132 0.135 0.139	0.142	0.146 0.149 0.153 0.156	96 0.160
		Stress Pe	Stress Period 1 (1987-1990):	0.365	Stress Period 2 (1991-1995):	0.263	Suess Period	Suess Period 3 (1996-2000):	0.155	Suess Period 4 (2001-2005):	0.135	Stress Period 5 (2006-2010):	0.153
No Growth		0.419 0.393	3 0.367 0.474	0.474	0.474 0.474 0.474 0.474 (0.474	0.474 0.474	0.474 0.474	0.474	0.474 0.474 0.474 0.474	0.474	0.474 0.474 0.474 0.474	74 0.474
		Stress Pe	Stress Period 1 (1987-1990):	0.427	Sucss Period 2 (1991-1995):	0.474	Stress Period	Stress Period 3 (1996-2000):	0.474	Stress Period 4 (2001-2005):	0.474	Stress Period 5 (2006-2010):	0.474
NEW BERN													_
Two-percent Growth 8	10.431	3.609 3.609 3.802	3.802 4.100	4.300	3.812 3.889 3.966 4.046	4.126	4.208 4.293	4.379 4.467	4.555	4,647 4,739 4,835 4,931	5.029	5.131 5.232 5.338 5.443	43 5.553
		Stress Pe.	Stress Period 1 (1987-1990):	3.953	Suess Period 2 (1991-1995):	3.968	Stress Period	Stress Period 3 (1996-2000):	4.380	Stress Period 4 (2001-2005):	4.836	Stress Period 5 (2006-2010):	5.339
Linear Growth		3.609 3.609	3.802 4.100	4.300	3.812 4.214 4.312 4.410	4.507	4.606 4.703	4.801 4.899	4.996	5.095 5.193 5.290 5.389	5.486	5.585 5.683 5.780 5.879	926 \$ 62
		Stress Pe	Stress Period 1 (1987-1990):	3.953	Suess Period 2 (1991-1995);	4.251	Stress Period	Stress Period 3 (1996-2000):	4.801	. Stress Period 4 (2001-2005):	5.291	Stress Period 5 (2006-2010):	5.781
No Growth		3.609 3.609	3.802 4.100	4.300	3.812 3.812 3.812 3.812	3.812 3	3.812 3.812	3.812 3.812	3.812	3.812 3.812 3.812 3.812	3.812	3.812 3.812 3.812 3.812	12 3.812
		Stress Pe	Stress Period I (1987-1990):	3.953	Suess Period 2 (1991-1995).	3.812	Stress Period	Stress Period 3 (1996-2000):	3.812	Stress Period 4 (2001-2005):	3.812	Sucss Period 5 (2006-2010);	3.812
						-							

# of wells Yield	5851d 5851d 5851d 5851d	0661A 63	P1991 P1992 P1993 P1994 P19	P1995 P1996	8661A Z661A	000ZA 6661A	2002 F2002 E2002 F20024 F2005	902 P2006	P2007 P2008 P2009	9 P2010
3.026	0.600 0.613 0.622 0.635	5 0.648	0.663 0.673 0.686 0.700 0.7	0.715 0.732	0.746 0.757	0.772 0.787	0.805 0.820 0.837 0.855 0.8	0.870 0.887	0.906 0.923 0.942	12 0.964
	Stress Period 1 (1987-1990):	0.630	Suess Period 2 (1991-1995): 0.6	0.687	Stress Period 3 (1996-2000):	900): 0.759	Suess Period 4 (2001-2005): 0.837		Stress Period 5 (2006-2010):	0.924
	0.600 0.613 0.622 0.635	5 0.648	0.657 0.670 0.683 0.692 0.7	0.705 0.7	0.718 0.727 0.740	0.753 0.762	0.775 0.788 0.797 0.810 0.823	123 0.832	0.845 0.858 0.867	0.880
	Stress Period 1 (1987-1990):	0.630	Stress Period 2 (1991-1995): 0.6	0.681	Stress Period 3 (1996-2000):	000): 0.740	Stress Period 4 (2001-2005): 0.799		Stress Period 5 (2006-2010):	0.856
	0.600 0.613 0.622 0.635	5 0.635	0.635 0.635 0.635 0.635 0.6	0.635 0.635	0.635 0.635	0.635 0.635	0.635 0.635 0.635 0.635 0.635	35 0.635	0.635 0.635 0.635	\$ 0.635
	Stress Period 1 (1987-1990);	0.626	Sucas Period 2 (1991-1995): 0.6	0.635	Stress Period 3 (1996-2000):	000): 0.635	Suess Period 4 (2001-2005): 0.635		Stress Period 5 (2006-2010):	0.635
11.725	3.453 3.715 3.843 4.202	12 4.317	4.293 4.380 4.467 4.557 4.6	4.647 4.739	4.833 4.931	5.031 5.133	5.234 5.337 5.444 5.554 5.663	5.776	5.893 6.011 6.130	0 6.253
	Stress Period 1 (1987-1990):	4.019	Suess Period 2 (1991-1995): 4.4	4.469	Stress Period 3 (1996-2000):	000): 4.933	Stress Period 4 (2001-2005): 5.4	5.446 S	Stress Period 5 (2006-2010):	6.013
	3.453 3.715 3.843 4.202	2 4.317	4.293 4.462 4.589 4.858 5.2	5.203 5.549	5.893 6.254	6.661 7.068	7.475 7.882 8.288 8.694 9.102	9.509	9.914 10.322 10.727	7 11.134
	Stress Period 1 (1987-1990);	4.019	Suess Period 2 (1991-1995); 4.6	4.681	Stress Period 3 (1996-2000):	000): 6.285	Stress Period 4 (2001-2005): 8.288		Stress Period 5 (2006-2010):	10.321
	3.453 3.715 3.843 4.202	2 4.317	4.293 4.293 4.293 4.293 4.2	4.293 4.293	4.293 4.293	4.293 4.293	4.293 4.293 4.293 4.293 4.293	93 4.293	4.293 4.293 4.293	3 4.293
	Stress Period 1 (1987-1990):	4.019	Stress Period 2 (1991-1995): 4.2	4.293	Suess Period 3 (1996-2000):	000): 4.293	Suess Period 4 (2001-2005); 4.293		Stress Period 5 (2006-2010):	4.293
0.000	0.214 0.219 0.222 0.227	7 0.232	0.236 0.241 0.247 0.251 0.2	0.256 0.261	0.267 0.271	0.277 0.282	0.288 0.295 0.299 0.305 0.312	0.318	0.325 0.331 0.338	8 0.345
	Stress Period 1 (1987-1990):	0.225	Stress Period 2 (1991-1995): 0.2	0.246	Stress Period 3 (1996-2000):	000): 0.272	Suess Period 4 (2001-2005): 0.300		Suess Period 5 (2006-2010):	0.331
	0.214 0.197 0.204 0.210	0 0.216	0.221 0.227 0.233 0.239 0.2	0.246 0.251	0.257 0.263	0.270 0.275	0.281 0.287 0.293 0.299 0.3	0.305 0.312	0.318 0.322 0.328	8 0.335
	Stress Period 1 (1987-1990):	0.202	Stress Period 2 (1991-1995); 0.2	0.233	Stress Period 3 (1996-2000):	000): 0.263	Stress Period 4 (2001-2005): 0.293		Stress Period 5 (2006-2010):	0.323
	0.214 0.214 0.214 0.214	4 0.214	0.214 0.214 0.214 0.214 0.2	0.214 0.2	0.214 0.214 0.214	0.214 0.214	0.214 0.214 0.214 0.214 0.2	0.214 0.214	0.214 0.214 0.214 0.214	4 0.214
	Stress Period 1 (1987-1990):	0.214	Stress Period 2 (1991-1995): 0.2	0.214	Stress Period 3 (1996-2000):	000): 0.214	Suess Period 4 (2001-2005); 0.214		Stress Period 5 (2006-2010):	0.214
2.016	1.055 0.880 0.706 0.531	1 0.541	0.553 0.564 0.574 0.586 0.5	0.598 0.610	0.621 0.634	0.646 0.660	0.674 0.686 0.701 0.715 0.7	0.729 0.744	0.758 0.774 0.789	9 0.805
	Stress Period 1 (1987-1990):	0.664	Stress Period 2 (1991-1995): 0.5	0.575	Stress Period 3 (1996-2000):	000): 0.634	Stress Period 4 (2001-2005): 0.701		Stress Period 5 (2006-2010):	0.774
	1.055 0.880 0.706 0.531	1 0.356	0.182 0.007 0.000 0.000 0.0	0.000 0.000	0.000 0.000	0.000 0.000	0.0 0000 0000 0000 0000	0.000 0.000	0.000 0.000 0.000	00000 01
	Stress Period 1 (1987-1990):	0.618	Stress Period 2 (1991-1995): 0.0	0.038	Stress Period 3 (1996-2000):	000): 0.000	Stress Period 4 (2001-2005): 0.0	0.000	Stress Period 5 (2006-2010):	0.000
	1.055 0.880 0.706 0.531	1 0.531	0.531 0.531 0.531 0.531 0.5	0.531 0.531	0.531 0.531	0.531 0.531	0.531 0.531 0.531 0.531 0.5	0.531 0.531	0.531 0.531 0.531	1 0.531
	Stress Period 1 (1987-1990):	0.662	Stress Period 2 (1991-1995): 0.5	0.531	Suess Period 3 (1996-2000):	000): 0.531	Suess Period 4 (2001-2005): 0.531	_	Suess Period 5 (2006-2010):	0.531
0.000	0.123 0.126 0.128 0.131	1 0.133	0.136 0.139 0.141 0.144 0.1	0 147 0.150	0.153 0.156	0.160 0.163	0.166 0.169 0.172 0.176 0.17	0.179 0.182	0.187 0.190 0.194	94 0.198
	Stress Period 1 (1987-1990):	0.130	Stress Period 2 (1991-1995): 0.1	0.141	Suess Period 3 (1996-2000):	000): 0.156	Stress Period 4 (2001-2005): 0.1'	0.172 S	Stress Period 5 (2006-2010):	0.190
	0.123 0.132 0.138 0.145	5 0.151	0.157 0.163 0.170 0.176 0.1	0.182 0.18	0.188 0.194 0.200	0.206 0.213	0.219 0.225 0.231 0.238 0.244	0.250	0.255 0.262 0.268	8 0.274
	Stress Period 1 (1987-1990):	0.141	Suess Period 2 (1991-1995): 0.1	0.170	Suess Period 3 (1996-2000):	000): 0.200	Stress Period 4 (2001-2005): 0.231		Stress Period 5 (2006-2010):	0.262
	0.123 0.123 0.123 0.123	3 0 123	0.123 0.123 0.123 0.123 0.1	0.123 0.123	0.123 0.123	0.123 0.123	0.123 0.123 0.123 0.123 0.123	23 0.123	0.123 0.123 0.123	13 0.123
	Stress Period 1 (1987-1990):	0.123	Stress Period 2 (1991-1995): 0.1	0.123	Stress Period 3 (1996-2000):	000): 0.123	Stress Period 4 (2001-2005): 0.123		Stress Period 5 (2006-2010):	0.123
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ACKNOWLEDGMENTS

The Division of Water Resources requested and received reviews of this document by professionals from other agencies. These comments are valuable and we acknowledge the reviewers' efforts. The Division appreciates comments from Ron Coble and Jodie Eimers of the U.S. Geological Survey and members of the Groundwater Section staff of the North Carolina Division of Environmental Management.